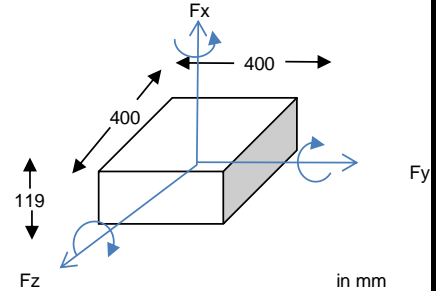


Laminated Elastomeric Bearing Calculation Based On EN 1337-3:2005 ( TYPE - C )

Calculation sheet		DATE -31/10/2021	Pages: 3	ID :
Client	M/s. NMDC	LOCATION	Size - 400 x 400 x 119mm	
Project	NMDC - THUMAYRIYAH ACCESS BRIDGE	Qty - 20nos		

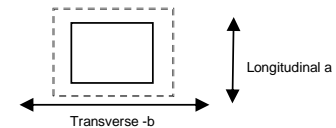
**BEARING DIMENSIONS**

a	Overall Width	mm	400.0
b	Overall Length	mm	400.0
c	Edge Cover of Elastomer	mm	6.0
a <sub>e</sub>	Effective Width	mm	388.0
b <sub>e</sub>	Effective Length	mm	388.0
n <sub>i</sub>	Number of inner Elastomer Layers		8.0
t <sub>i</sub>	Thickness of an inner Layer	mm	10.0
n <sub>o</sub>	No. of Outer Cover Layer		0.0
t'	Thickness of outer Cover Layer -	mm	0.0
n <sub>r</sub>	No. of reinforcing plates		7.0
t	Thickness of reinforcing plates	mm	2.7
C <sub>checker</sub>	Thickness of Top plate	mm	10.0
C <sub>checker</sub>	Thickness of Bottom plate combined	mm	10.0
h <sub>e</sub>	Actual thickness of Elastomer	mm	80.0
h	Overall thickness of Bearing	mm	119



**ELASTOMER PROPERTIES**

H	Nominal Hardness acc to EN 1337	IRHD	60.0
G <sub>l</sub>	long term shear modulus	N/mm <sup>2</sup>	0.90
G <sub>s</sub>	short term shear modulus / dynamic	N/mm <sup>2</sup>	0.90
E <sub>b</sub>	bulk modulus	N/mm <sup>2</sup>	2000.0
Cc	Compression Stiffness as per design	kN/mm	657.6



**DESIGN CALCULATIONS**

DESIGN LOADS			SLS	ULS				
Vertical Loads (kN)	V <sub>p</sub>	permanent	310	310				
	V <sub>l</sub>	live /seismic	590	880				
	V <sub>min</sub>	minimum	165	165				
	V <sub>d</sub>	design load = V <sub>p</sub> + V <sub>l</sub>	900	1190	<b>&lt;- Max Design Load</b>			
Horizontal Loads (kN)	H <sub>pb</sub>	permanent // to length b - Transverse Force	0	0				
	H <sub>lb</sub>	live /seismic //to length b - Transverse Force	20	12	<b>&lt;- Max Horizontal Transverse Force.</b>			
	H <sub>pa</sub>	permanent // to width a - Longitudinal Force	0	0				
	H <sub>la</sub>	live /seismic //to width a - Longitudinal Force	30	40	<b>&lt;- Max Horizontal Longitudinal Force.</b>			
DISPLACEMENTS & ROTATION			SLS	ULS				
Disp. in (mm)	δ <sub>pa</sub>	permanent disp // to width a - Longitudinal	6.0	9.0				
	δ <sub>pb</sub>	permanent disp // to length b - Transverse	0.0	0.0				
	δ <sub>pa</sub>	Live /reversible disp // to width a - Longitudinal	22.0	27.0				
	δ <sub>pb</sub>	Live /reversible disp // to length b - Transverse	20.0	12.0				
Rotation	α <sub>pa</sub>	Longitudinal permanent rotation	0.0004	0.0006				
	α <sub>pb</sub>	Transverse permanent rotation	0.0001	0.0002				
	α <sub>la</sub>	Longitudinal live/seismic rotation	0.0025	0.0033				
	α <sub>lb</sub>	Transverse live/seismic rotation	0.0006	0.0009				
	α <sub>ma</sub>	Longitudinal maximum rotation		0.0039	<b>&lt;- Max Longitudinal Rotation Value</b>			
	α <sub>mb</sub>	Transverse maximum rotation		0.0011	<b>&lt;- Max Transverse Rotational Value</b>			
SHAPE FACTOR			SLS	ULS				
S	Shape Factor		9.700	9.700				
A <sub>r</sub>	Effective plan area (mm <sup>2</sup> )		150544	150544				
l <sub>p</sub>	Force Free Parameter (mm)		1552	1552				
DISPLACEMENTS DUE TO LIVE LOAD			SLS	ULS				
K <sub>d</sub>	dynamic stiffness (KN/mm)		1.69	1.69	<b>&lt;- Calculated Shear Stiffness Value</b>			
K <sub>s</sub>	static shear stiffness(KN/mm)		1.69	1.69				
δ <sub>la</sub>	permanent disp // width a (mm) - Longitudinal - Horizontal Load		6.00	9.00				
δ <sub>lb</sub>	permanent disp // length b (mm) - Transverse - Horizontal Load		0.00	0.00				
δ <sub>la</sub>	live/seismic disp // width a (mm) - Longitudinal		39.71	50.62				
δ <sub>lb</sub>	live/seismic disp // length b (mm) - Transverse		31.81	19.09				



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<b>DISPLACEMENT DUE TO SHEAR LOAD</b>		SLS	ULS	
$\delta_a$	displacement in direction width - a (mm) - Longitudinal	45.71	59.62	<- Longitudinal Displacement due to Horizontal force
$\delta_b$	displacement in direction length - b (mm) - Transverse	31.81	19.09	<- Transverse Displacement due to Horizontal force
<b>SHEAR STRAIN</b>		SLS	ULS	
$\epsilon_{qa}$	Design load strain // width a - Longitudinal	0.57	0.75	
$\epsilon_{qb}$	Design load strain // length b - Transverse	0.40	0.24	
$\epsilon_q$	resultant shear strain	0.70	0.80	
$\epsilon_{pv}$	permissible value for shear strain	0.70	1.00	
CHECKS $\epsilon_{pv} > \epsilon_q$		PASS	PASS	CHECK - 1
<b>DESIGN STRAIN DUE TO COMPRESSIVE LOAD</b>		SLS	ULS	
$A_r$	reduced $A_1$ (mm <sup>2</sup> ) area	120465	120007	
$\epsilon_{cl}$	Design Strain due to live load	0.84	1.26	
$\epsilon_{cp}$	Design Strain due to Permanent Load	0.44	0.44	
$\epsilon_{cd}$	Strain due to design load - long term G ( only for ULS cal )		1.70	
<b>DESIGN STRAIN DUE TO ANGULAR ROTATION</b>		SLS	ULS	
$\epsilon_{al}$	Design Strain due to live load	0.26	0.35	
$\epsilon_{cp}$	Design Strain due to Permanent Load	0.04	0.42	
<b>MAXIMUM DESIGN STRAIN - sum of strains</b>		SLS	ULS	
$K_{Ll}$	type loading factor for live loads - Safety factor (1 or 1.5)	1.5		
$K_{Lp}$	type loading factor for all others - Safety factor	1.4		
$K_L$	type loading factor		1.0	
$Y_m$	partial safety factor	1.40	1.00	
$\epsilon_u$	maximum permissible value	7.00	7.00	
$\epsilon_t$	sum of strains	3.40	2.92	
$\epsilon_{pv}$	Sum of all strain - permissible value as per En 1337-3 2005	5.0	7.00	
CHECK $\epsilon_t < \epsilon_{pv}$		PASS	PASS	CHECK - 2
<b>ROTATION LIMITATION</b>		SLS	ULS	
$K_r$	rotation factor	3.00	3.00	
$z_l$	live load deflection of an individual inner layer (mm)	0.11	0.17	
$z_p$	perm load deflection of an individual inner layer (mm)	0.06	0.06	
$\sum z$	total vertical deflection of bearing(mm)	1.37	1.81	
$z_{min}$	Min vertical deflection of bearing required to allows rotation	0.47	0.65	
CHECK $\sum z > z_{min}$		PASS	PASS	CHECK - 3
<b>FIXING OF BEARING</b>		SLS	ULS	
$\sigma_m$	average comp stress due to V d ( N/mm <sup>2</sup> )	7.47	9.92	
$\sigma_{cdmin}$	min comp stress due to min load ( N/mm <sup>2</sup> )	1.37	1.37	
$\sigma_{pv}$	permissible value	3.00	3.00	
$\mu_{ec}$	friction coefficient between concrete & checkered plates	0.5	0.5	
$H_a$	design horizontal load // to width a (kN) -Longitudinal	77	101	
$H_b$	design horizontal load // to length b (kN) - Transverse	54	32	
$H$	resultant horizontal force (kN)	94	106	
$H_{rc}$	resistance force due to $\mu_{ec}$ (kN)	155	155	
CHECK $\sigma_m < 15,20$ Mpa		PASS	PASS	CHECK - 4
CHECK $H_{rc} > H$ ( Required only in case of Top/Bottom Checker plate )		PASS	PASS	CHECK - 5
<b>BUCKLING STABILITY</b>		SLS	ULS	
$\sigma_d$	average comp stress due to V d ( N/mm <sup>2</sup> )	7.47	9.92	
$\sigma_{pv}$	permissible value ( this calculation uses long term G )	28.23	28.23	
CHECK $\sigma_{pv} > \sigma_d$		PASS	PASS	CHECK - 6
<b>INTERNAL MS STEEL PLATE / SHIM THICKNESS</b>		SLS	ULS	
$f_y$	yield stress of the steel ( N/mm <sup>2</sup> )	260	260	
$K_p$	Stress correction factor	1.3	1.3	
$K_h$	induced tensile stresses factor	1.0	1.0	
$Y_m$	partial safety factor	1.3	1.3	
$t_{s1}$	minimum thickness of steel plate (mm) Calculated	1.0	1.3	
$t_{s2}$	minimum thickness of steel plate (mm)	2.0	2.0	
$t$	Thickness of reinforcing plates (mm)	2.7	2.7	
CHECK $t > t_{s1}$ and $t > t_{s2}$		PASS	PASS	CHECK - 7



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5.3.3.7 FORCES, MOMENTS ACTING ON THE STRUCTURE		SLS	ULS				
Rxy	Resultant of forces resisting the translatory movement in KN	94.32	106.02				
Mb	Restoring Moment due to rotation about an axis through the centre of the bearing , // to length (b) in KN/mtr	4.90	4.90				
Ma	Restoring Moment due to rotation about an axis through the centre of the bearing , // to width (a) in KN/mtr	17.37	17.37				

Yellow columns - values to be entered

Disclaimer: Ptfе- Teflon laminated bearing sizes, load details, bearing construction details and corresponding calculations are proprietary information designed M/s. POLYMET INDUSTRIES RAK – UAE based on EN 1337-3:2003 and 2005 for above mentioned Project and carries pending Middle East & UAE patents. These information's should not be reproduced or copied without our written consent and to be used by the Client/Consultant for the Project which it is proposed. Should not be copied or passed over to other manufacturers for reference or pricing and violation of the same can lead to litigation by International Arbitration which will be based in Dubai – UAE. Information given here is for general and can be changed without notice. Teflon® Fluor polymer resins are registered trademark of DuPont™ and Neoprene® registered trade mark of Bayer ™ for details on this disclaimer & our STD terms & conditions please contact us by email: polymet@pretread.com or pretread@eim.ae

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